

Effect of Mixing Enhancement Devices on Turbulence in Separate Flow Nozzles

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Work presented here was accomplished through the efforts of a team of skilled technicians, engineers, researchers, and managers at NASA Glenn Research Center and its industry partners, General Electric Aircraft Engines and Pratt & Whitney. Dr. Mark Wernet of NASA Glenn was key to PIV work presented here.

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AST Program

- NASA Pillar Goals
 - Reduce engine noise by 10dB in 10 years
 - Reduce engine noise by 20dB in 20 years
- Programs
 - Advanced Subsonic Technology (AST) 1994—2000
 - Airframe noise
 - Fan noise
 - Jet noise—Goal: 3EPNdB
 - Low—Mid Bypass Ratio, internally mixed nozzles
 - Mid—High Bypass Ratio, separate flow nozzles
 - » SFNT97 Test program
 - Base R&T (BASE) 2000—
 - Jet Noise Reduction
 - SFNT2K Test program



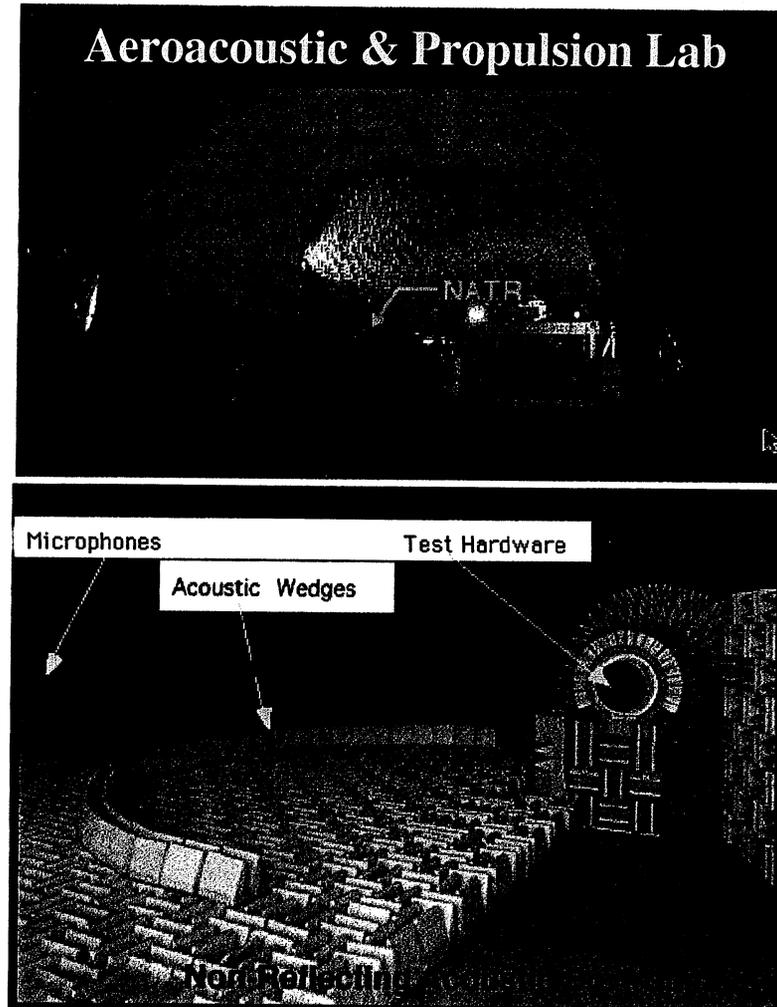
Test Programs SFNT97 and SFNT2K

- Collaborative test with GE, Pratt & Whitney as primes, Allison, Boeing as subcontractors
- Organization:
 - Industry and NASA brought in ideas
 - Industry designed and built hardware
 - NASA did testing at Glenn Research Center and ASE/FluiDyne Labs
 - Industry and NASA did analysis.
- Many noise reduction concepts screened, first analytically, then in acoustic tests.
- Best (and most interesting) measured using IR, Schlieren, Pt/Tt survey rakes, and phased arrays.
- NASA returned in 2000 (SFNT2K) with few additional concepts and PIV to better understand *why* reductions found or not found.



Facility

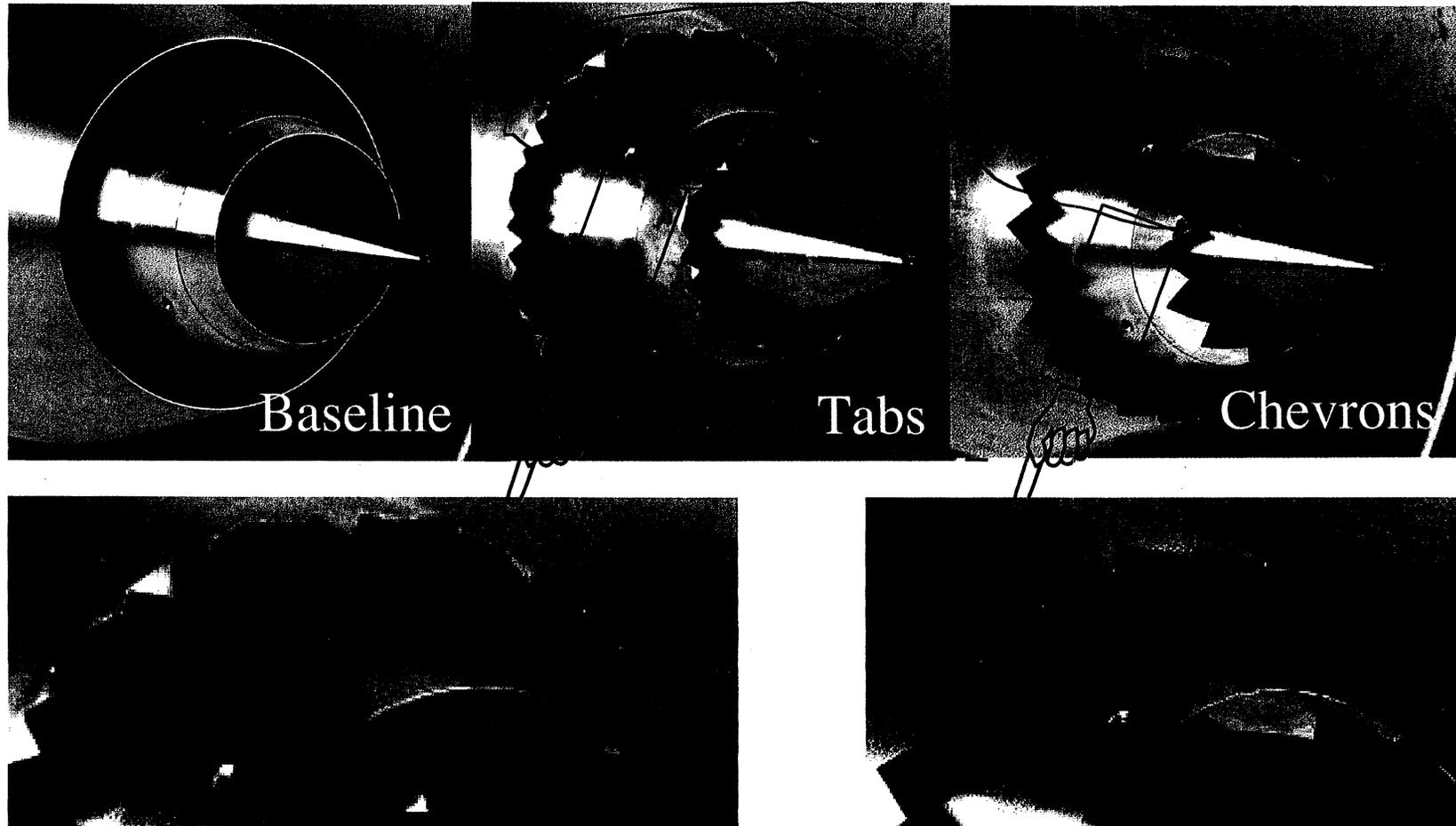
- 65ft. radius geodesic dome
- Anechoic environment
- Up to 0.3 Mach freestream
- Dual stream engine flow simulation
 - Core: 5lbm/sec@1500°R
 - Fan: 25lbm/sec@600°R
- Acoustic measurements
 - 26 1/4" B&K microphones at 50' R
 - 63 element 2D phased array
- Flow visualization
 - Infrared, Schlieren,
- Flow measurements
 - Pressure-Temperature survey rakes
 - Pressure-Sensitive Paint (PSP)
 - Particle Image Velocimetry (PIV)





Mixing Enhancement Nozzles

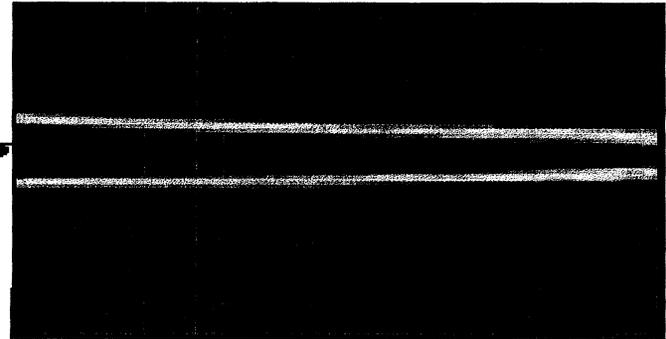
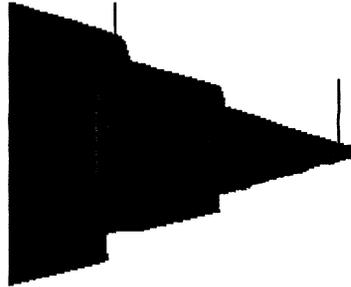
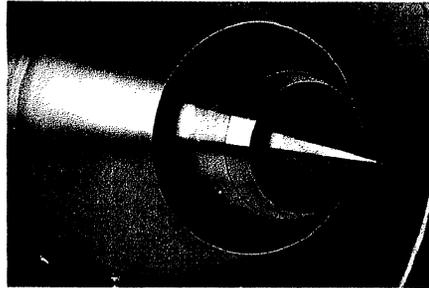
A few representatives of the 43 configurations studied in SFNT97.



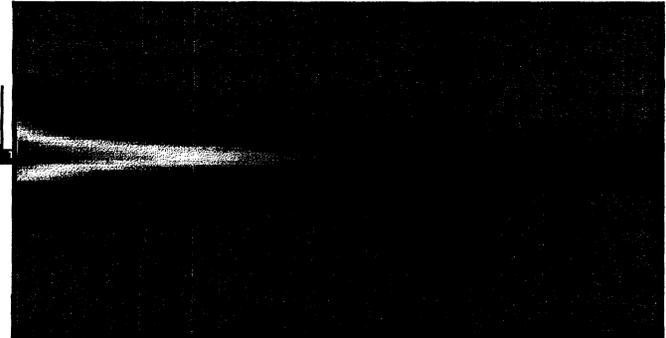
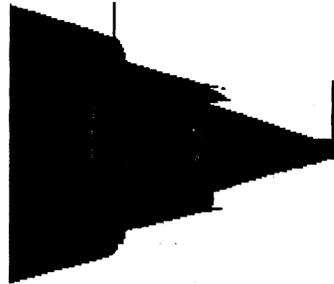
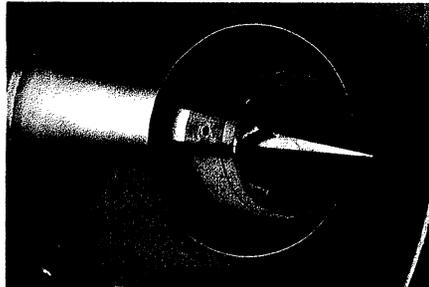


IR reductions

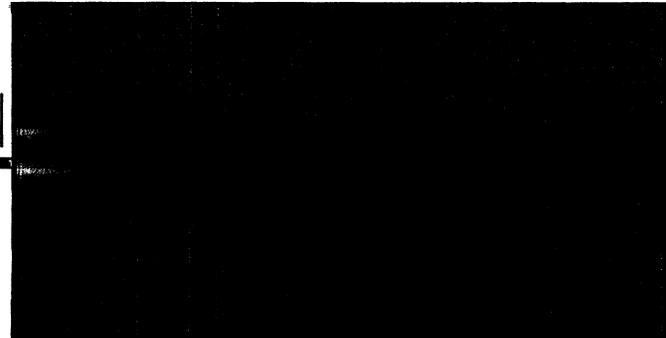
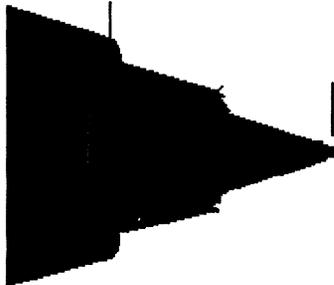
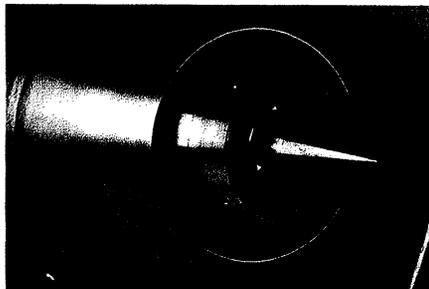
3BB



3AB



3TB



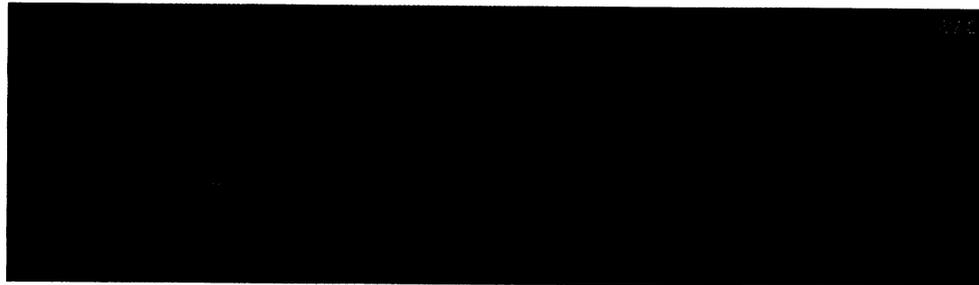


Schlieren of Chevrons

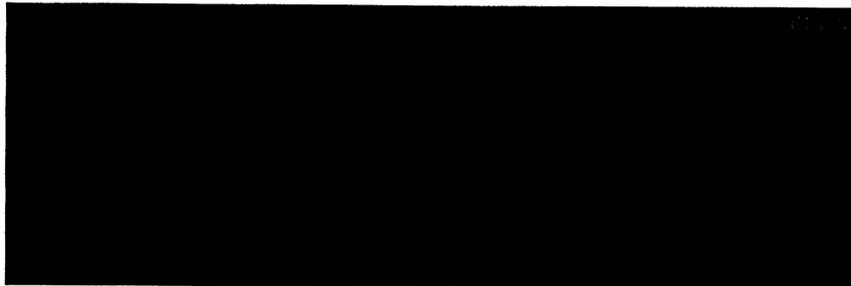
3BB



3AB



3TB

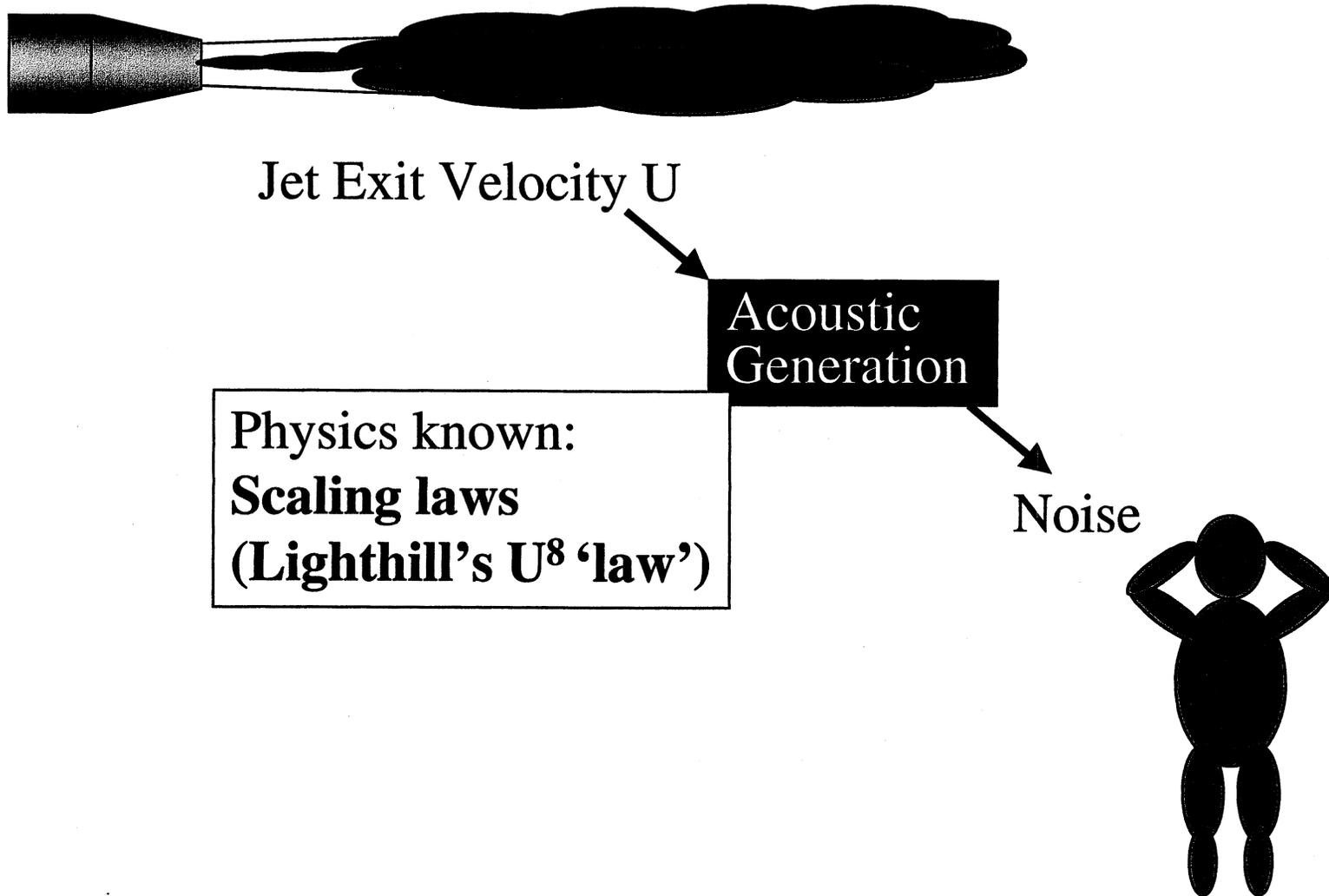


- Increased jet spread

- Axial streaks ('vortices')

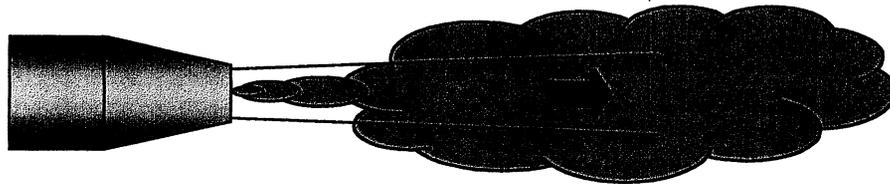


Aeroacoustics of Enhanced Mixing—Paradigm





Aeroacoustics of Enhanced Mixing—Reduction Paradigm

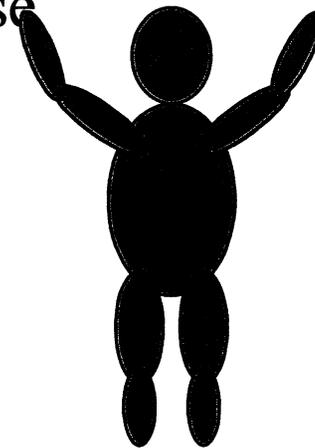


Lowering Effective Jet Velocity...

Acoustic
Generation

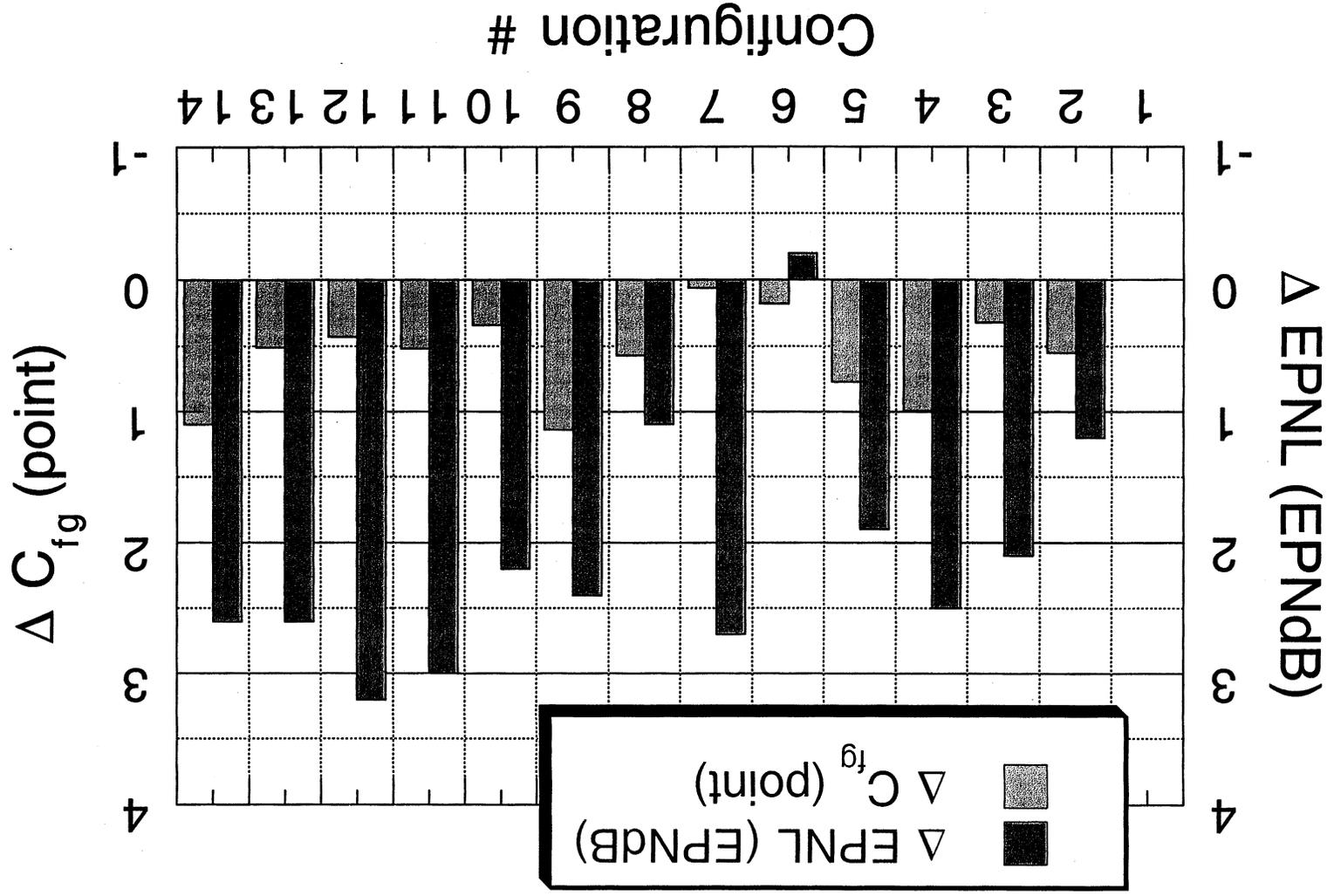
Physics known:
Scaling laws
(Lighthill's U^8 'law')

... Lowers Noise





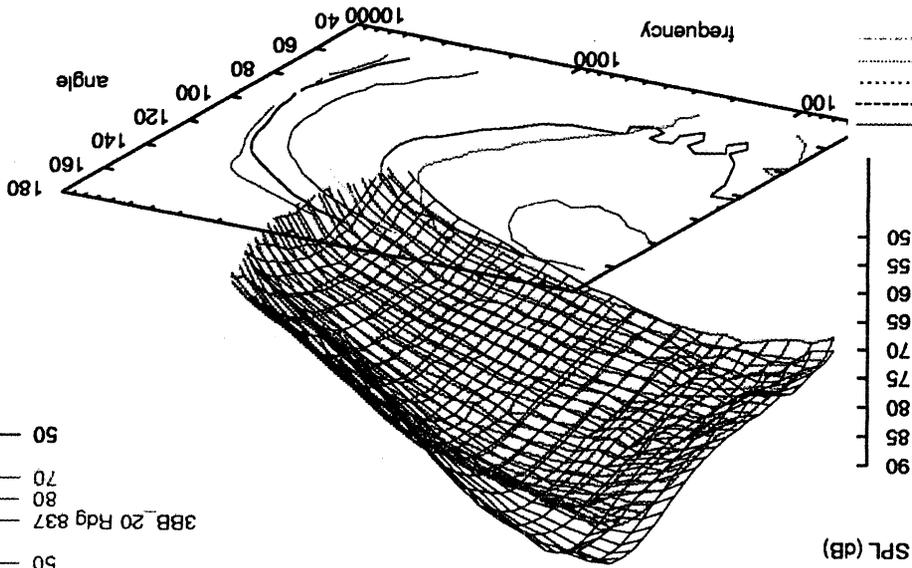
Acoustic and Thrust Performance of Enhanced Mixing Nozzles





Aeroacoustics of Enhanced Mixing—Data

3A12B_20 Rdg 778
 50
 60
 70
 80
 3BB_20 Rdg 837
 50
 60
 70
 80



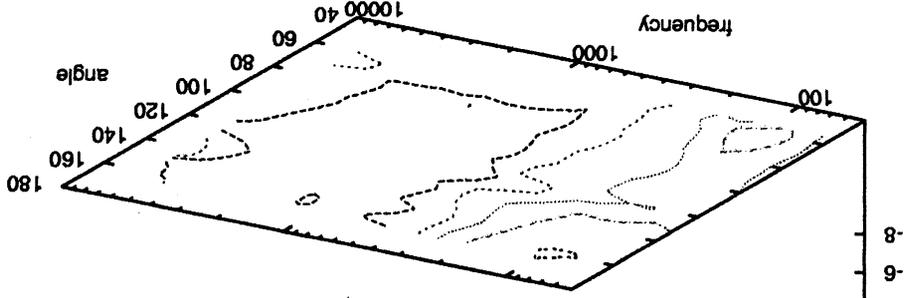
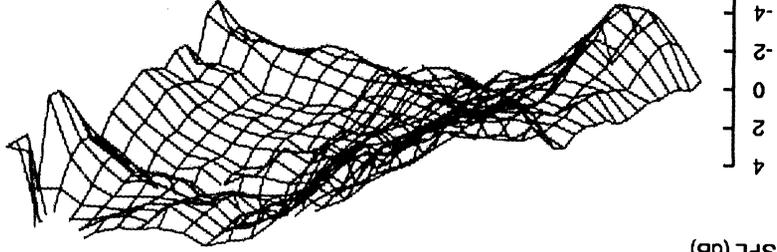
Net reduction is an optimization problem.

- Enhanced mixing by chevrons
 - Decreases low frequencies near jet axis.
 - Increases high frequencies.

90
85
80
75
70
65
60
55
50

3A12B_21 Rdg 777 - (3BB_21 Rdg 836)

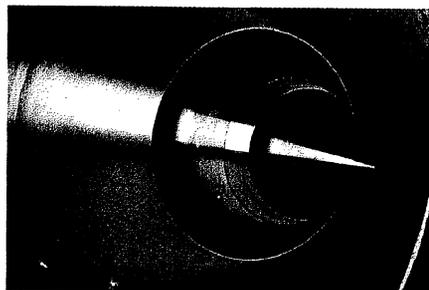
2
0
-2
-4
-8



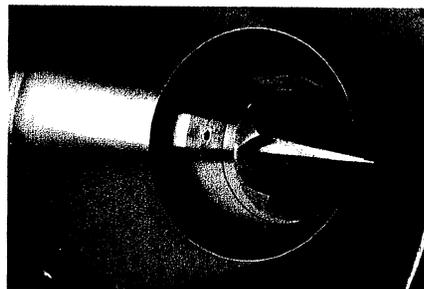


Enhanced Mixing == Less Noise?

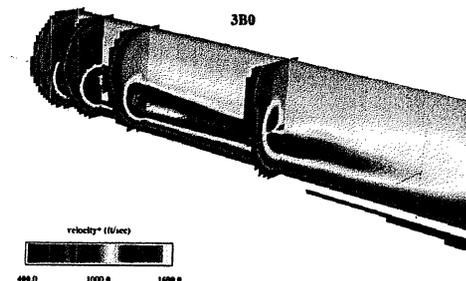
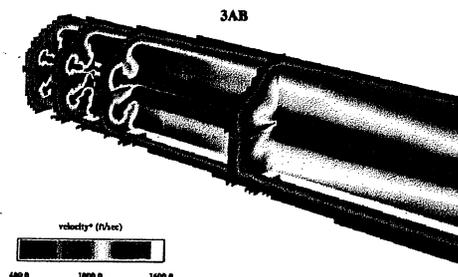
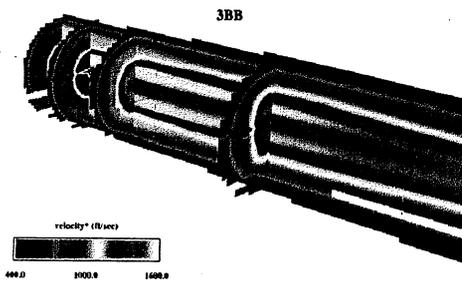
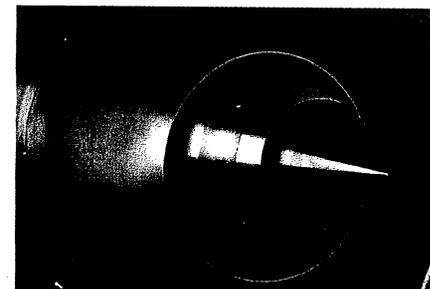
Baseline



Alternating Chevrons



Offset Bypass



Baseline
Nozzle technology being
manufactured on quietest jet
aircraft in late 1990's.

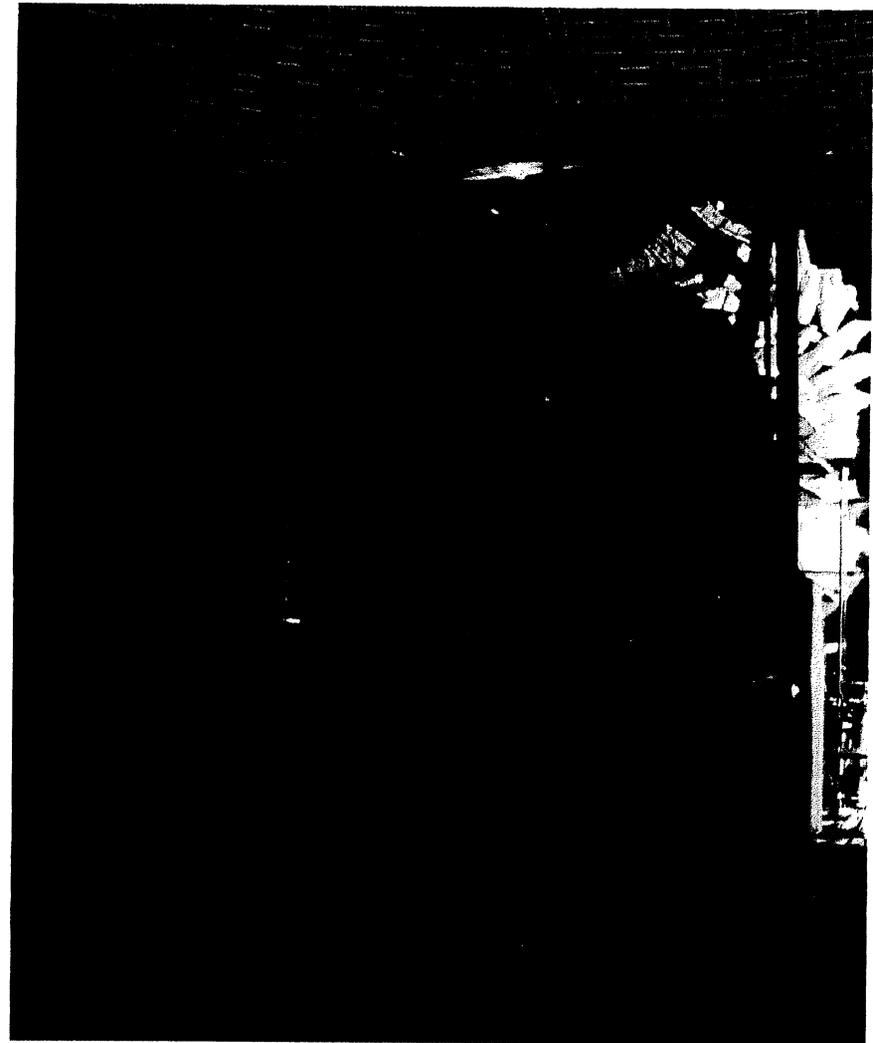
Quietest by 2.5EPNdB!
Good mixing reduced noise
sources without producing
additional sources!

Noisiest by 3EPNdB!
Good mixing, but method of
mixing introduced new noise
source!



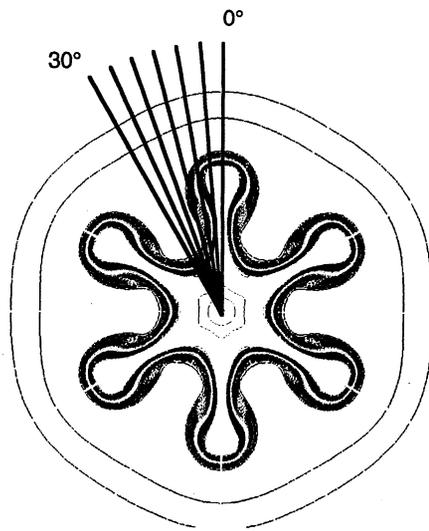
PIV Instrumentation

- Large Traversing frame setup to axially traverse
 - Laser and optics
 - 400mJ/pulse PIVdual-head laser
 - 0.2mm thick sheet
 - Two cameras
 - Dual frame PIV cameras
 - 2.5 μ s between pulses
 - Visual Background
- Seed
 - Core and fan flows
 - 0.7 μ m Al₂O₃
 - fluidized bed seeders injected in rig supply pipes
 - Freestream
 - 0.2 μ m oil droplets
 - commercial fogger injected at inlet to freejet tunnel.





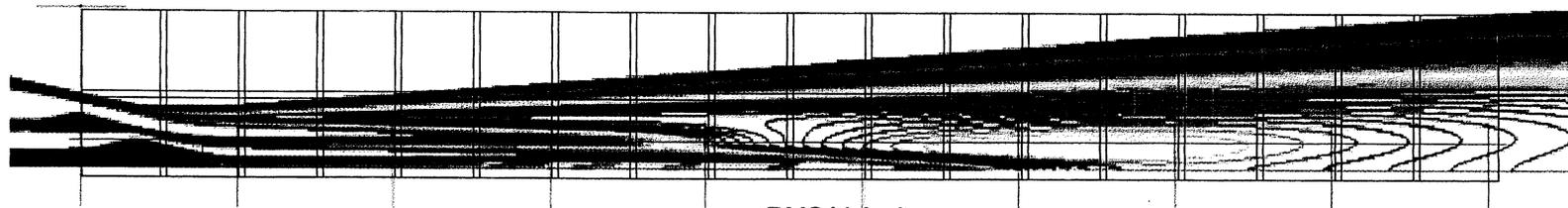
PIV Measurement Layout



Mean Velocity
 U (m/s)



0 250 500



RMS Velocity
 u' (m/s)



0 15 30

- 3BB:
 - one radial (x,r) plane
 - 10 × 1 fan diameters
- 3A12B/ 3T24B:
 - 7 radial planes (5° increment)
 - 10 x 1 fan diameters for 0°, 15°, 30°
 - 5 x 1 fan diameters for 5°, 10°, 20°, 25°
- 400 frames used in statistics at each location.



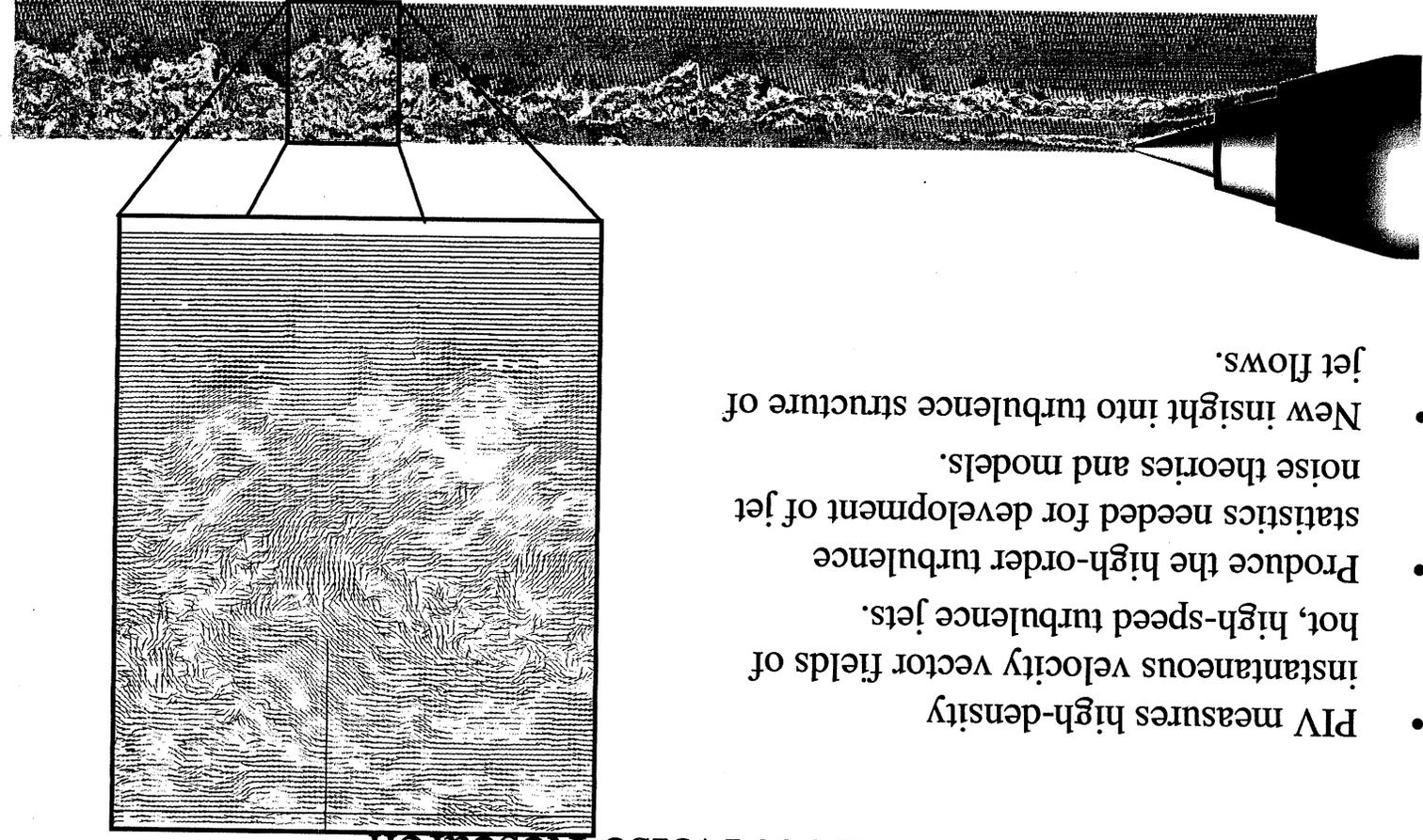
Flow conditions

- All data were taken at the same exhaust conditions:
 - $NPR_{core} = 1.68$, $T_{tcore} = 1500^{\circ}R$
 - $NPR_{fan} = 1.83$, $T_{tfan} = 600^{\circ}R$
 - Freejet Mach = 0.28
- This is an average take off flow condition.



PIV in Jet Noise Research

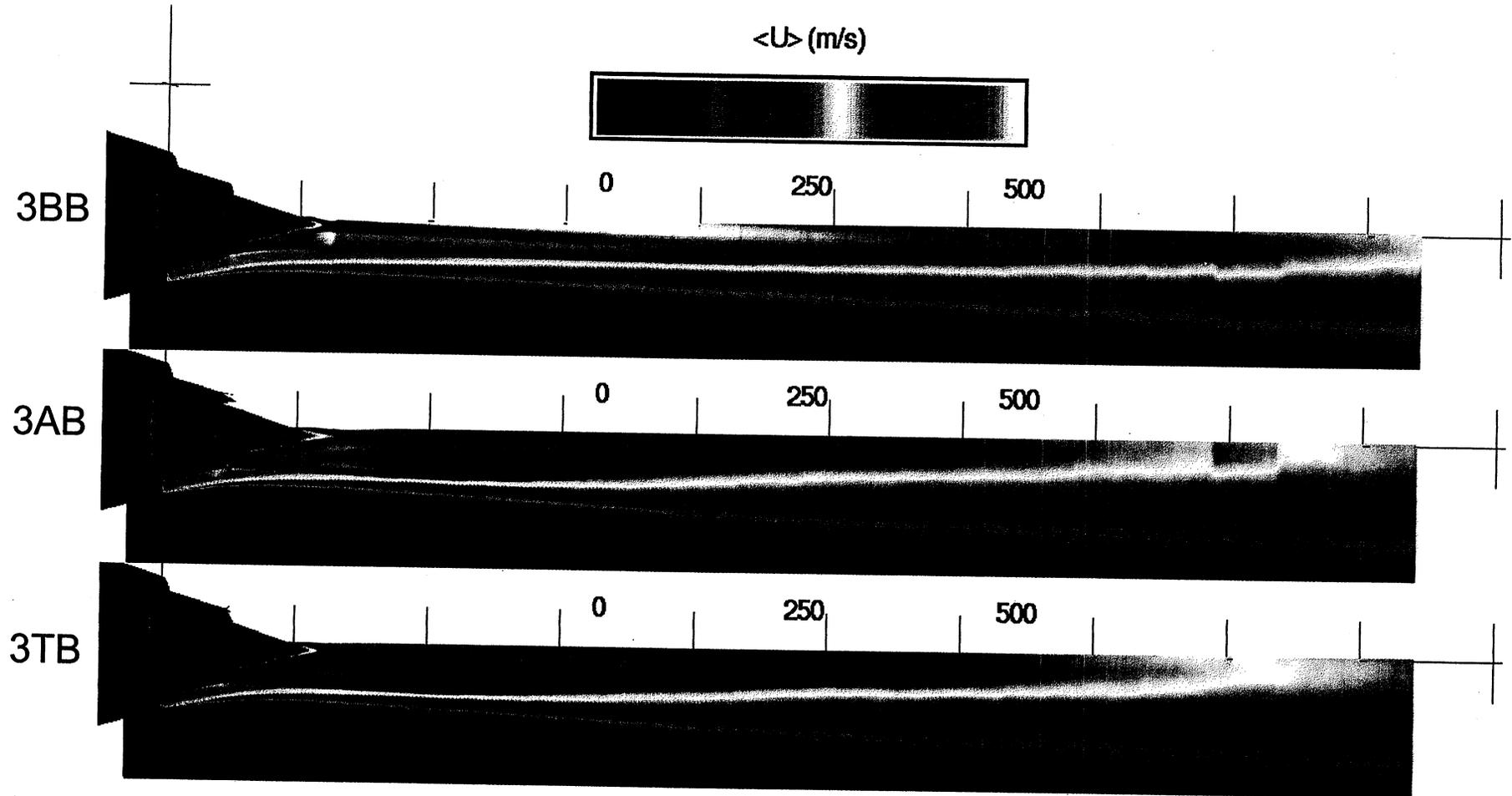
- PIV measures high-density instantaneous velocity vector fields of hot, high-speed turbulence jets.
- Produce the high-order turbulence statistics needed for development of jet noise theories and models.
- New insight into turbulence structure of jet flows.



Velocity vectors in axisymmetric separate flow nozzle at takeoff. Structure convection speed subtracted from vectors to enhance structures. 1080 by 120 vectors, 2.25mm/vector density.

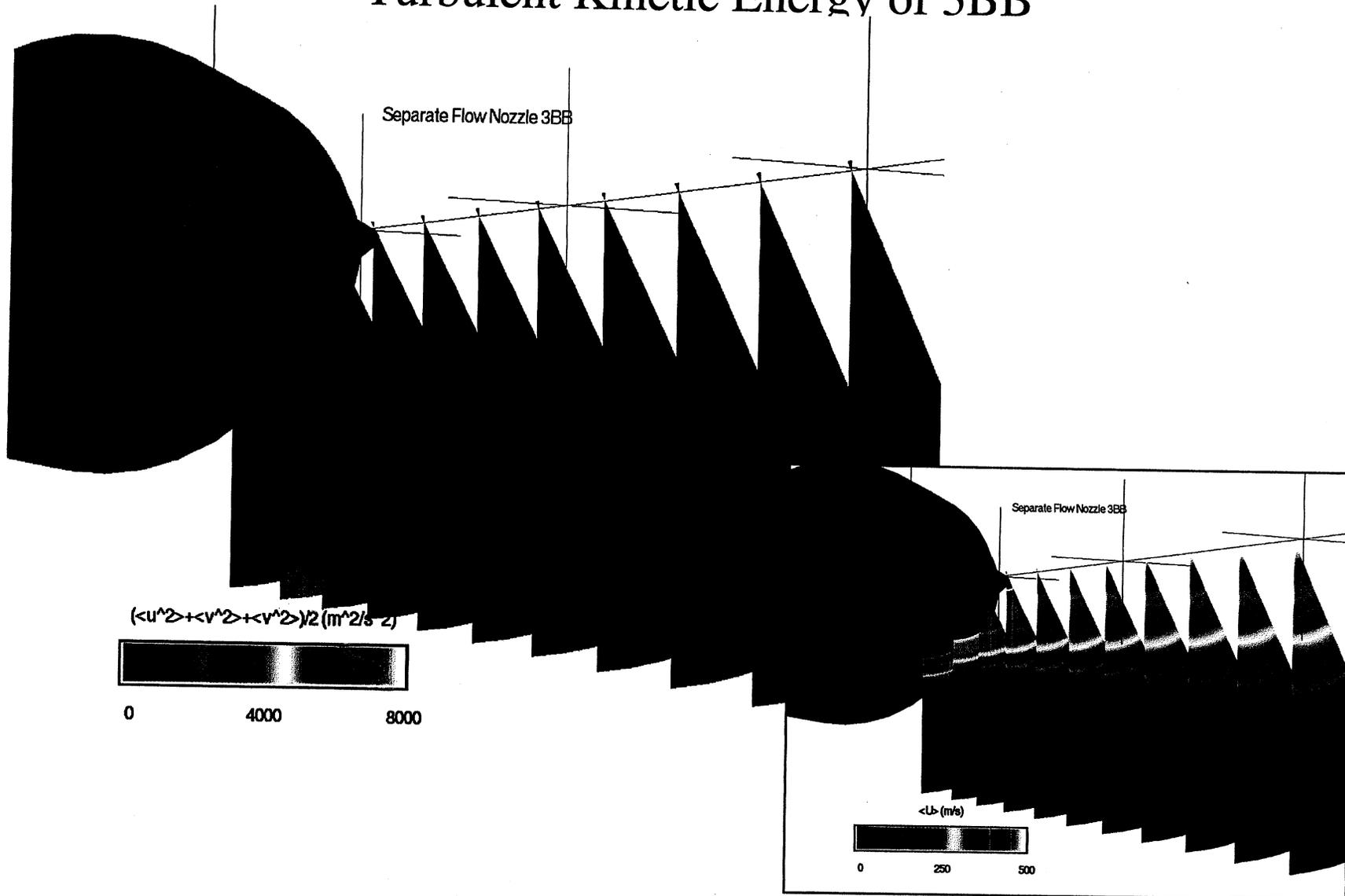


Mean Velocities



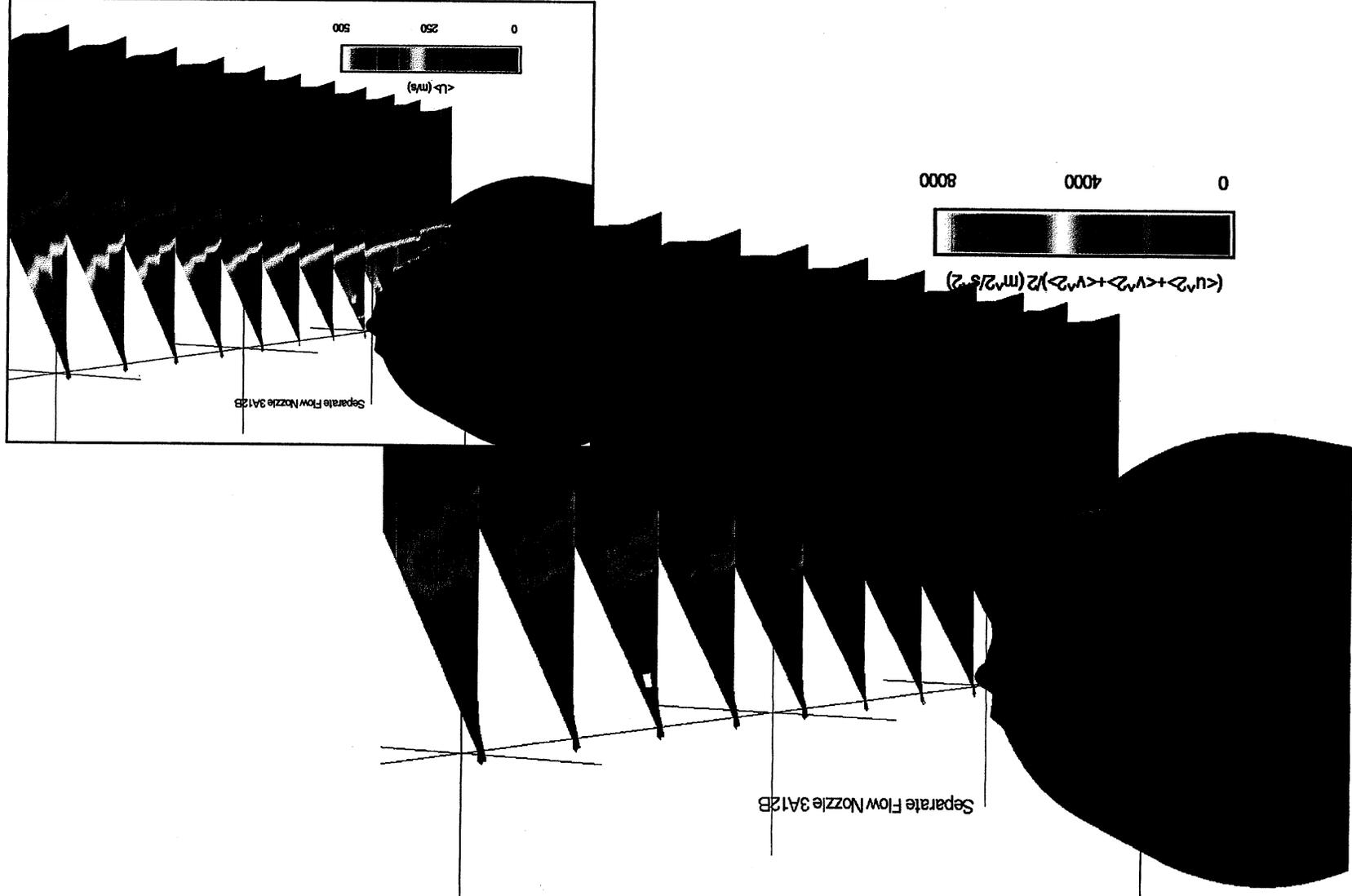


Turbulent Kinetic Energy of 3BB



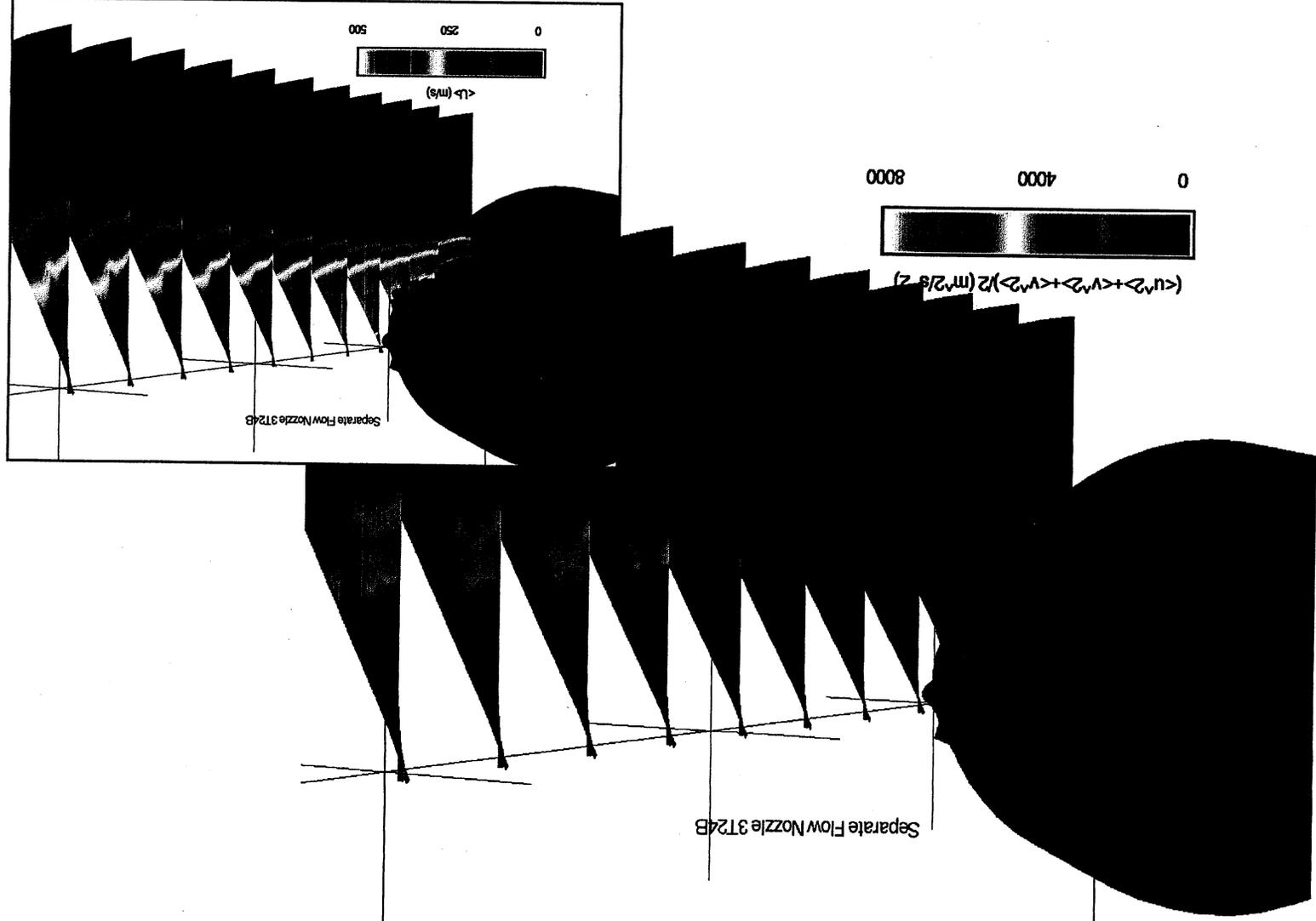


Turbulent Kinetic Energy of 3A₁B





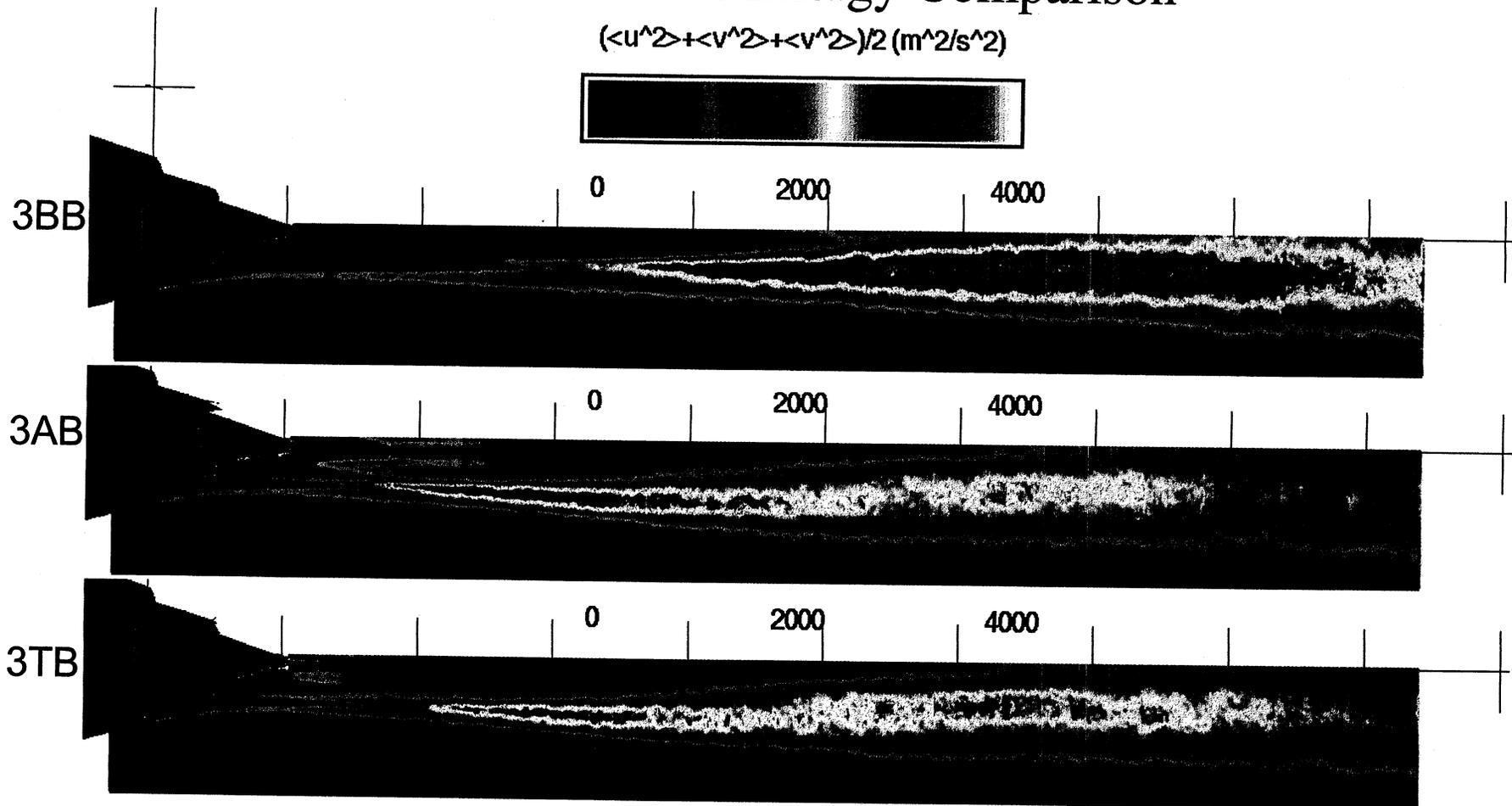
Turbulent Kinetic Energy of 3T²⁴B





Turbulent Kinetic Energy Comparison

$$(\langle u^2 \rangle + \langle v^2 \rangle + \langle w^2 \rangle) / 2 \text{ (m}^2/\text{s}^2)$$



Large reductions, especially in fully mixed region

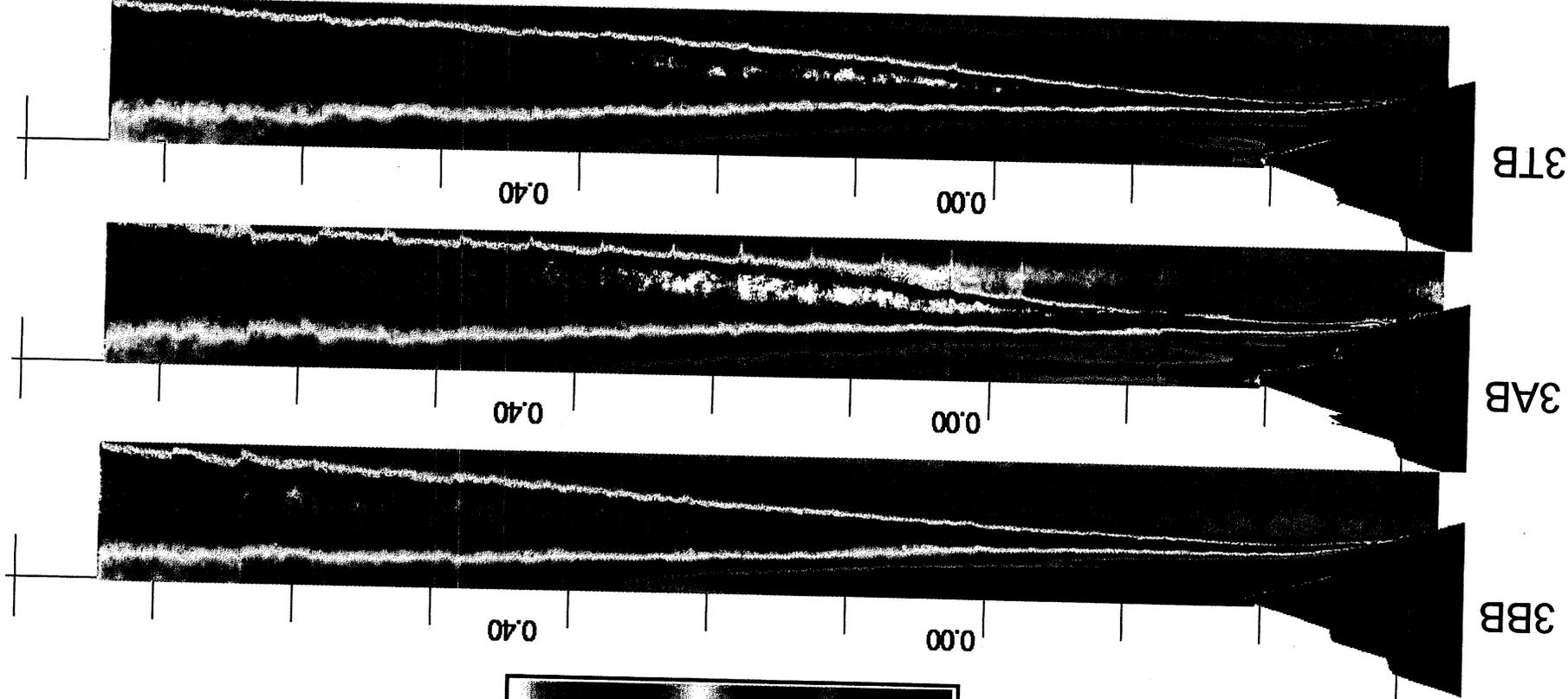
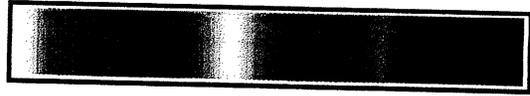
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Turbulence Intensity Comparison

$$\frac{\langle u'^2 \rangle}{U^2}$$

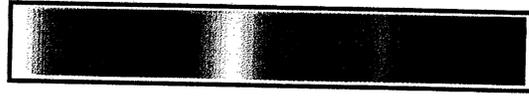


No reduction in intensity; if anything an increase upstream



Distribution of TKE by Component

$$\langle u'^2 \rangle / \langle v'^2 \rangle$$

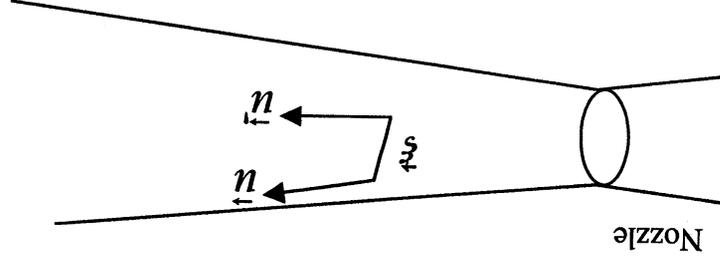


Higher value \Rightarrow more efficient sound conversion



Spatial Correlations of Velocity

- Spatial correlations needed to model turbulence beyond turbulent kinetic energy, a one-point measure.
- PIV ideally suited for this measurement, capturing instantaneous velocity fields over a region chosen to be larger than the correlation size.



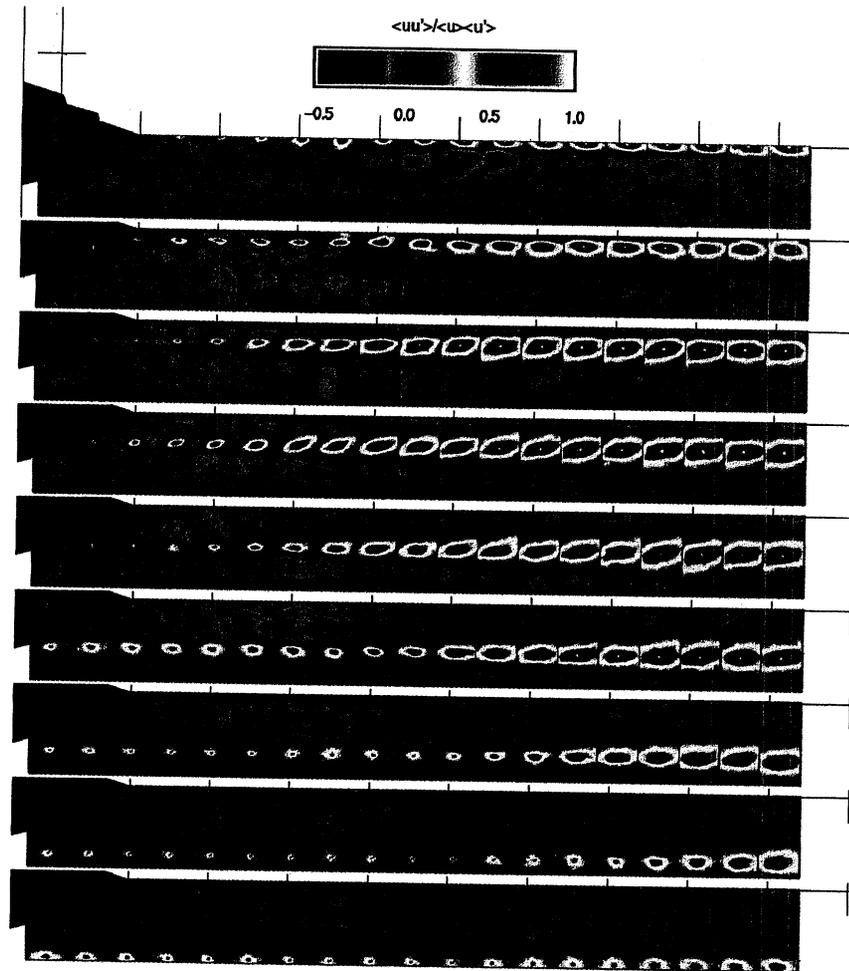
$$\tilde{R}_{ij}(\xi_k, \vec{x}) = \frac{\sqrt{\overline{u_i^2(\vec{x})} \overline{u_j^2(\vec{x})}}}{\overline{u_i(\vec{x} + \xi_k/2) u_j(\vec{x} - \xi_k/2)}}$$



Two-Point Correlations of uu'

3BB

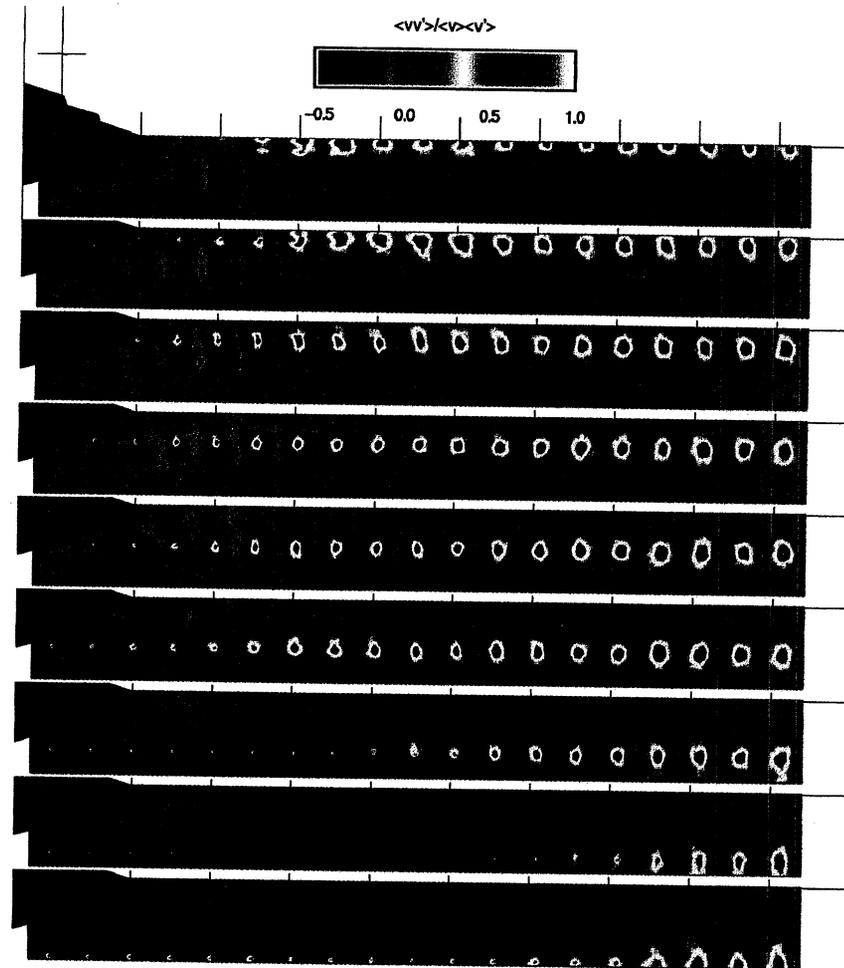
3BB





Two-Point Correlations of vv' 3BB

3BB

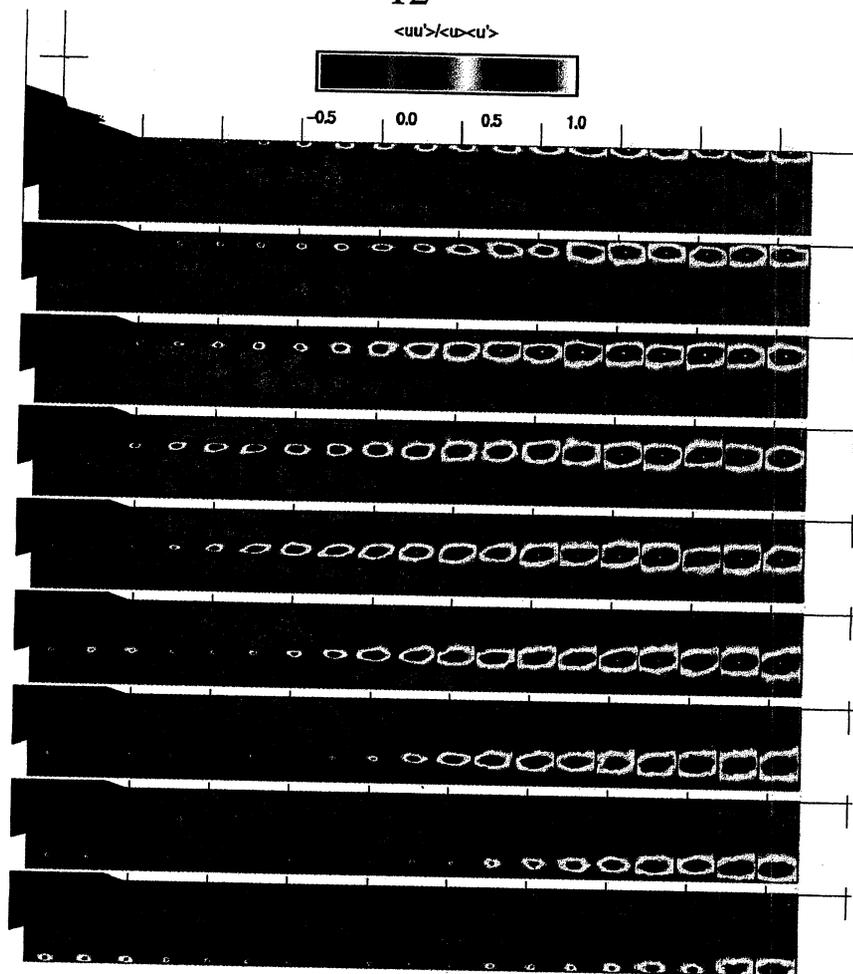




Two-Point Correlations of uu'

$3A_{12}B$

$3A_{12}B$

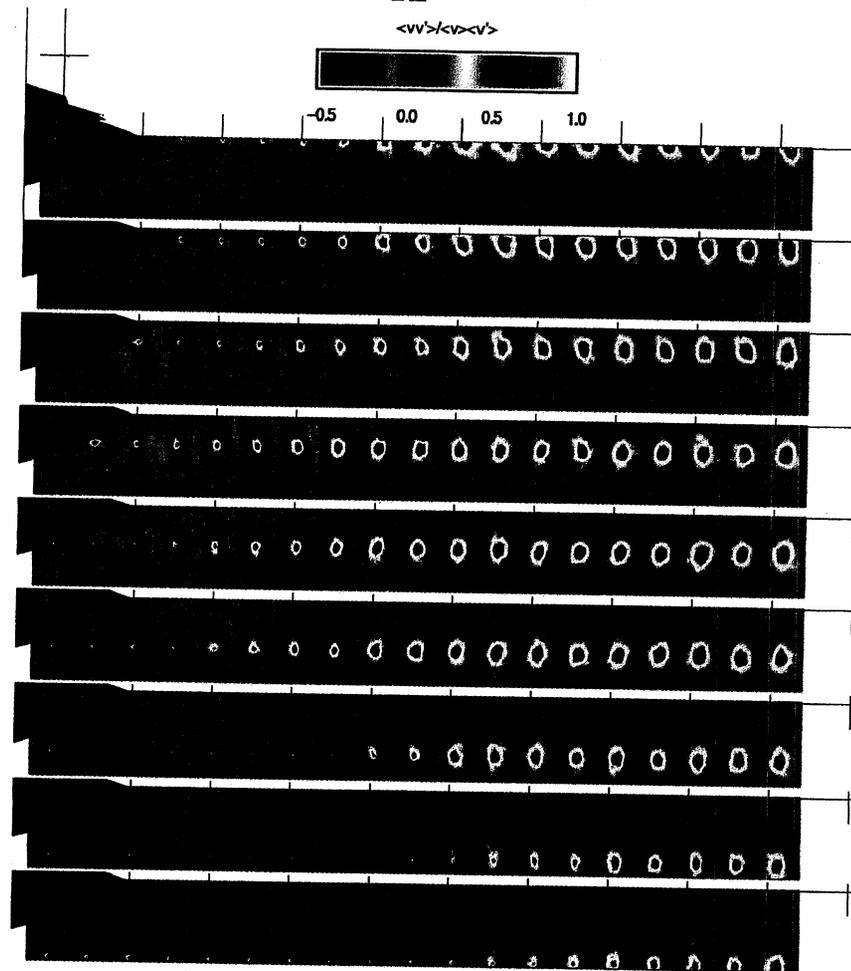




Two-Point Correlations of vv'

$3A_{12}B$

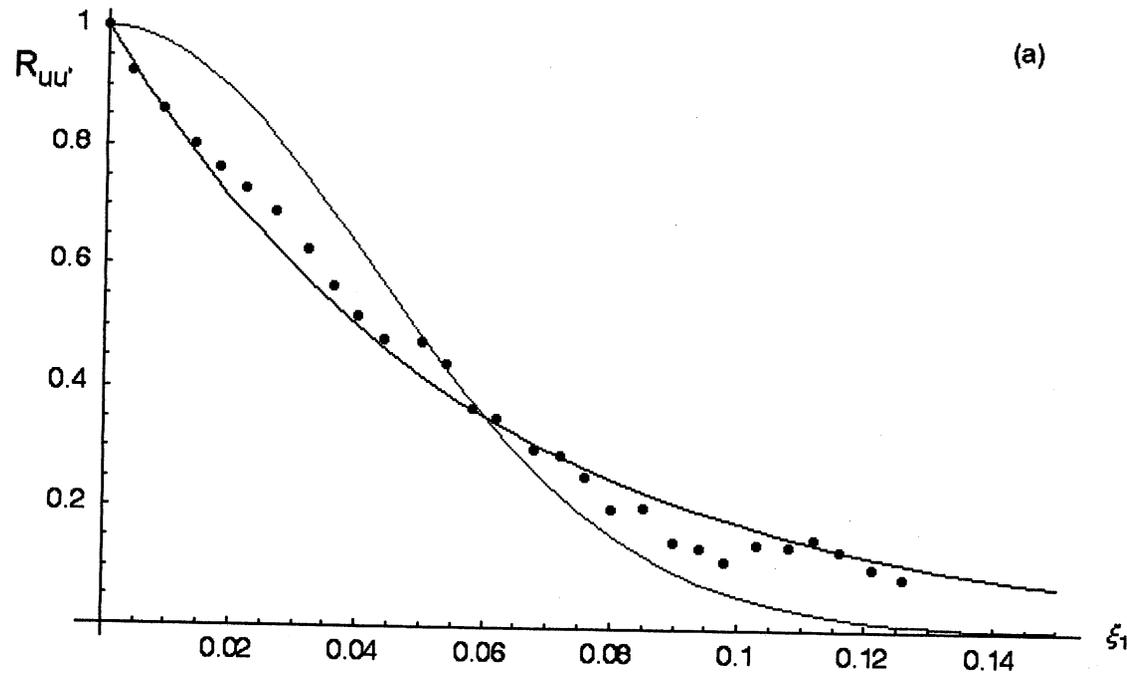
$3A_{12}B$





Fit of Spatial Correlation Data to Turbulence Models

- Modeling spatial correlations of velocity by form $\exp(-(\xi/L)^n)$.
- Usual model is Gaussian ($n=2$; in blue)
- Better fit for high Reynolds number is $n=1$ (black line)





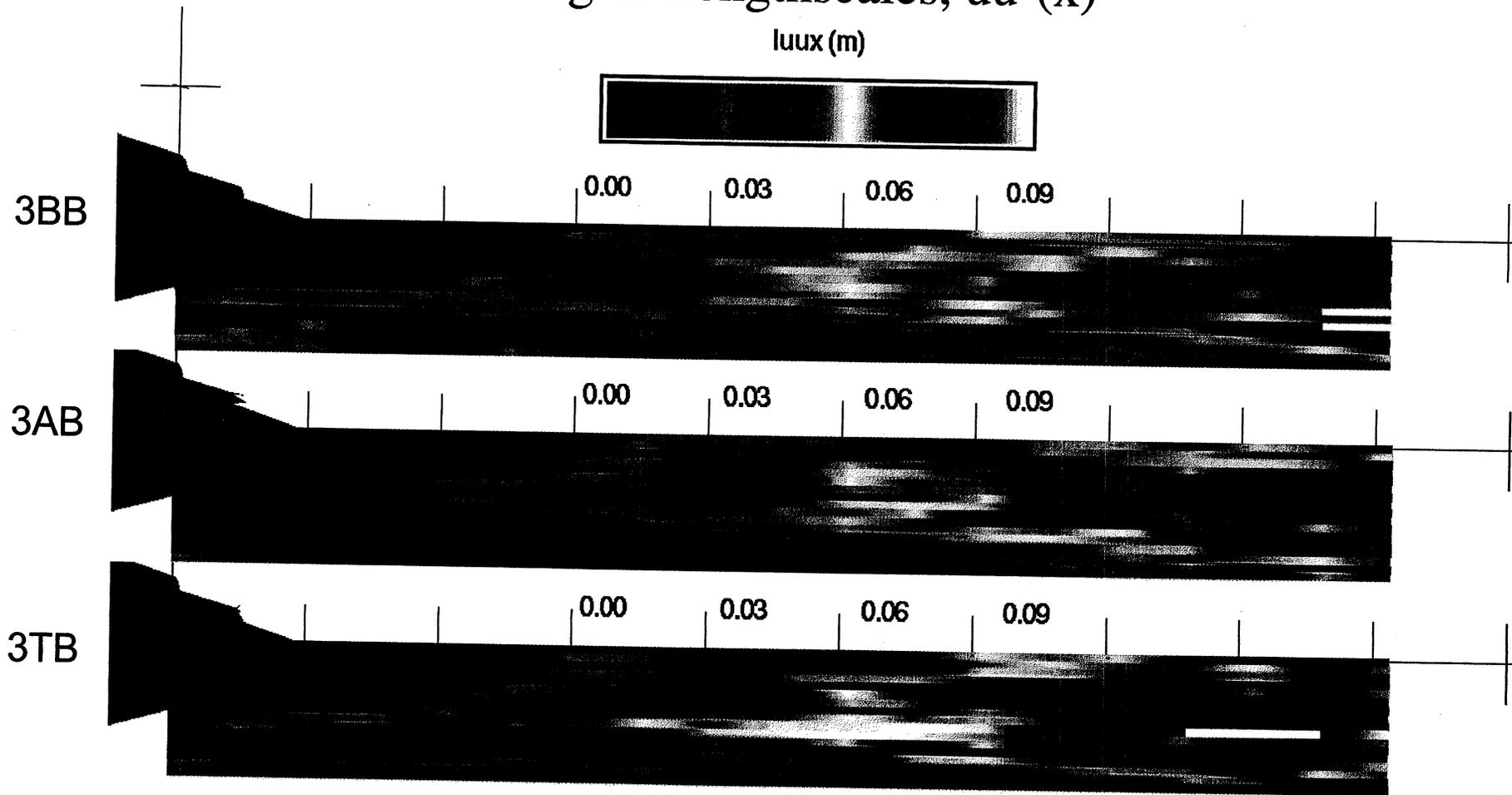
Integral Lengthscales

- Integral lengthscales are a measure of largest scale of turbulence, measure of peak in turbulence wavenumber spectrum.
- Integral lengthscales are used in jet noise modeling to estimate frequency of sound being produced by kinetic energy in that region.
- Estimate integral lengthscales from integral of curve fitted to data.

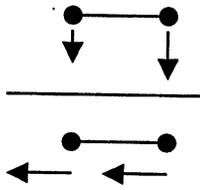
$$I u_i u_i, \xi_k (\vec{x}) = \int_0^{\infty} R_{ii} (\xi_k, \vec{x}) d\xi_k$$



Integral Lengthscales, $uu'(x)$

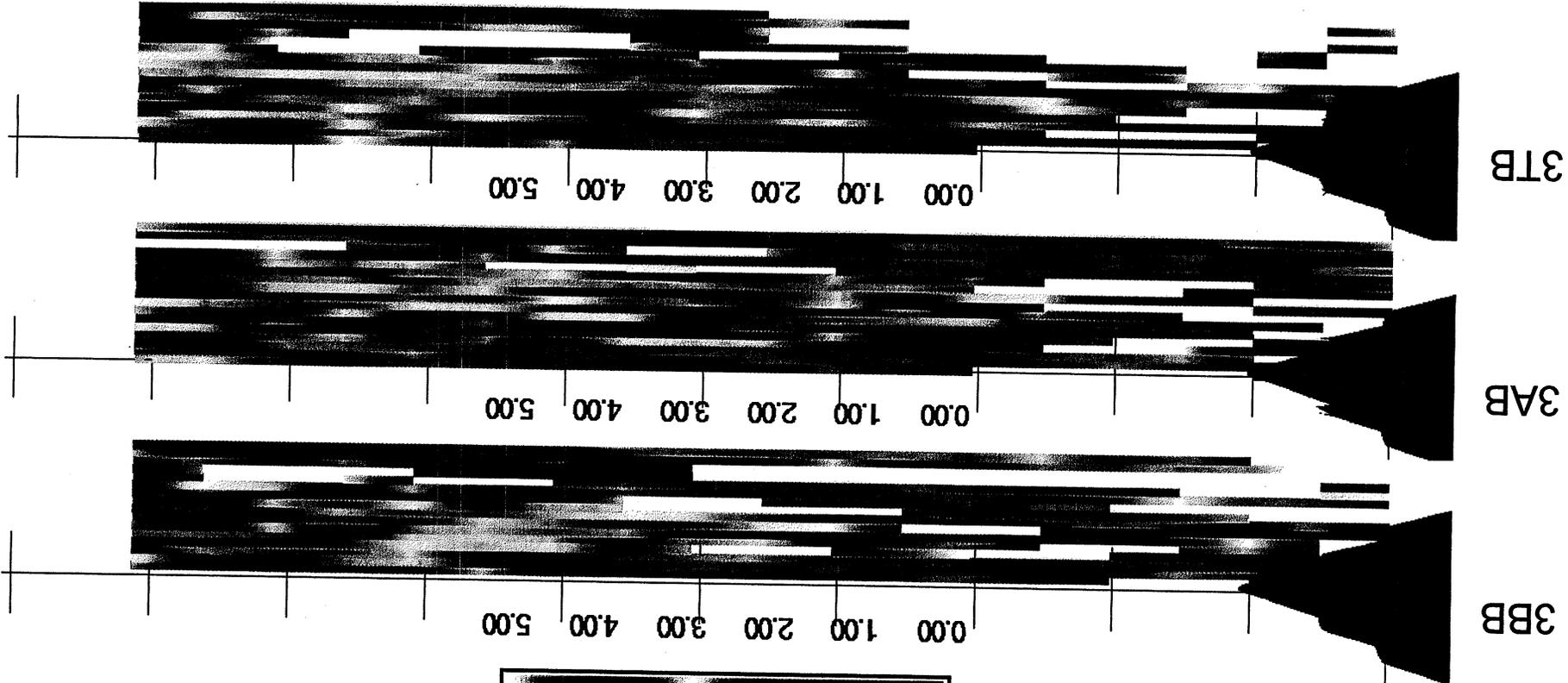
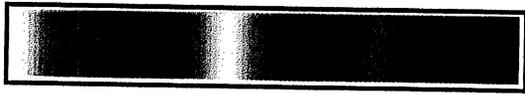


Lengthscales relatively unaffected by mixing enhancement



Ratio of Lengthscales in ξ_1

l_{ux}/l_{vx}

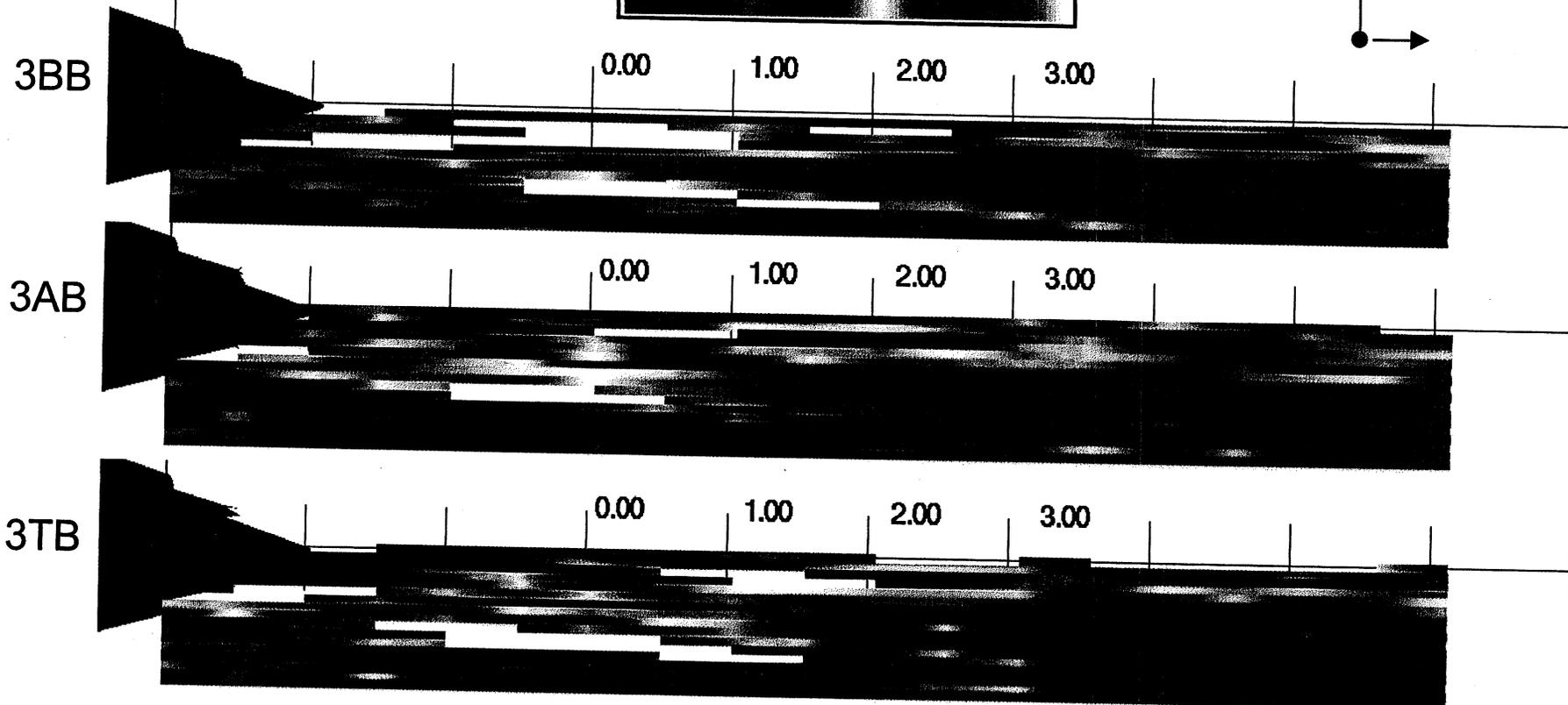
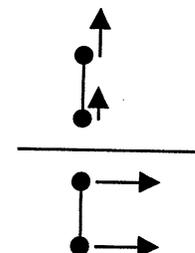


Equals 2 if isotropic; slightly more if axisymmetric



Ratio of Lengthscales in ξ_2

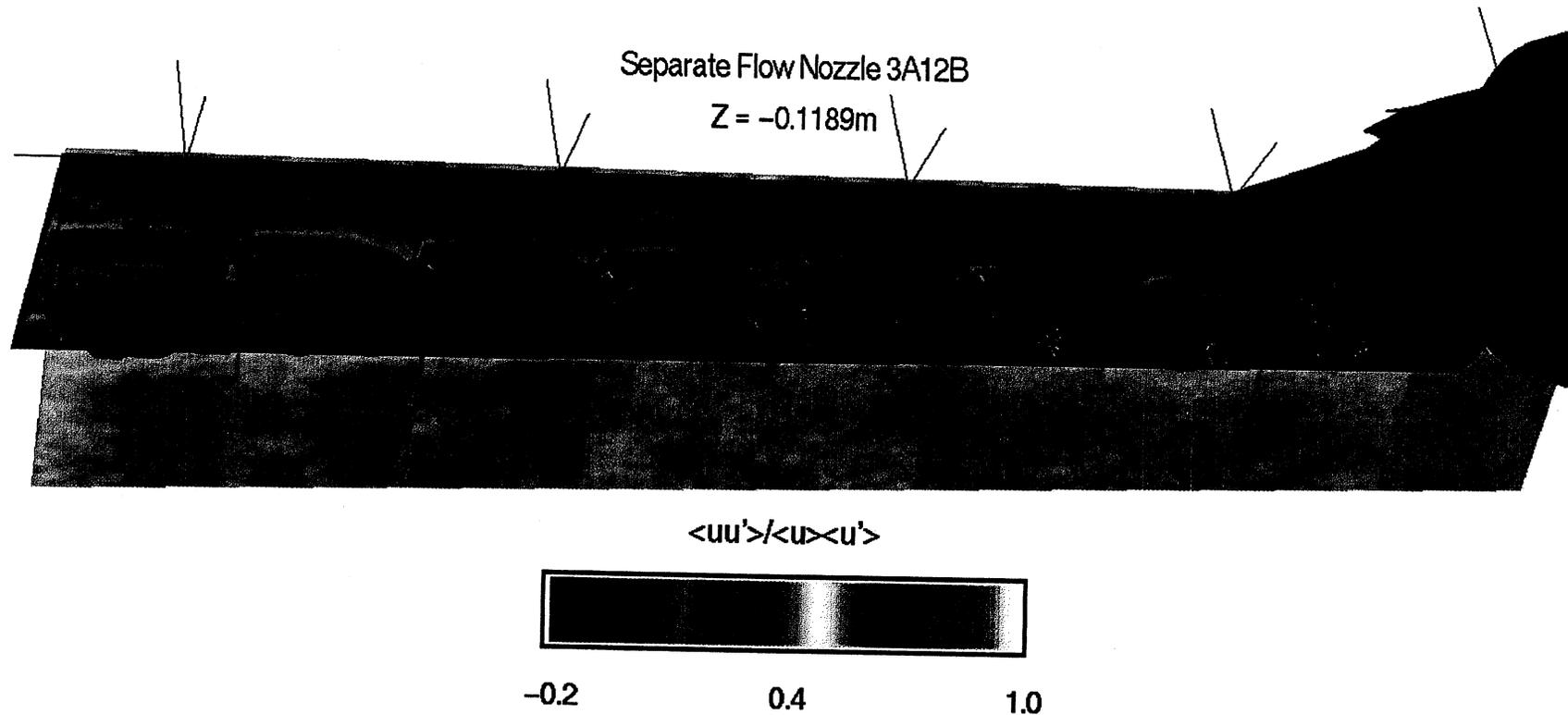
$$l_{vy}/l_{uy}$$



Expected to be 2 in either case, not nearly 1!



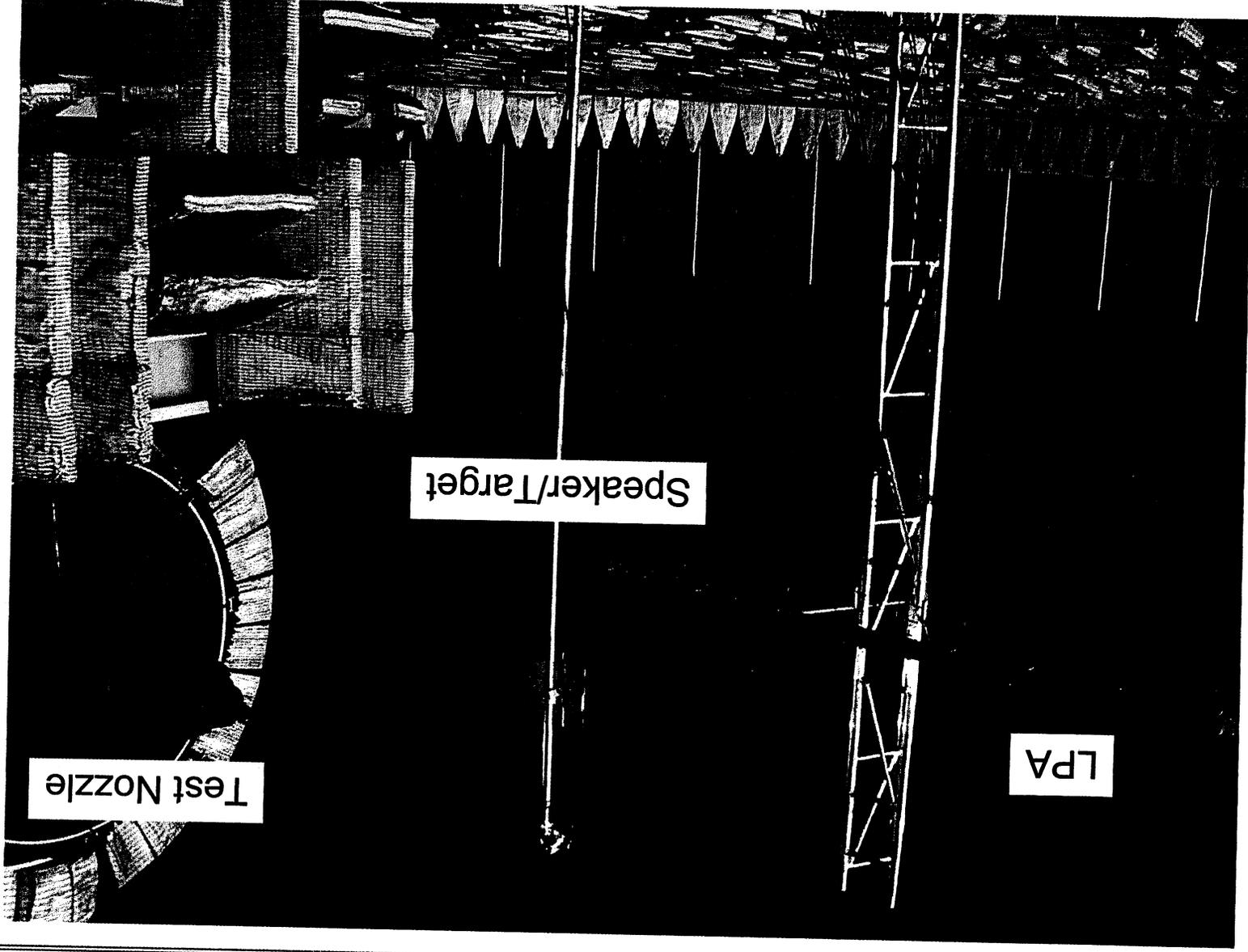
Two-Point Correlations



Spatial correlations are homogeneous, even in circumferential direction with chevrons

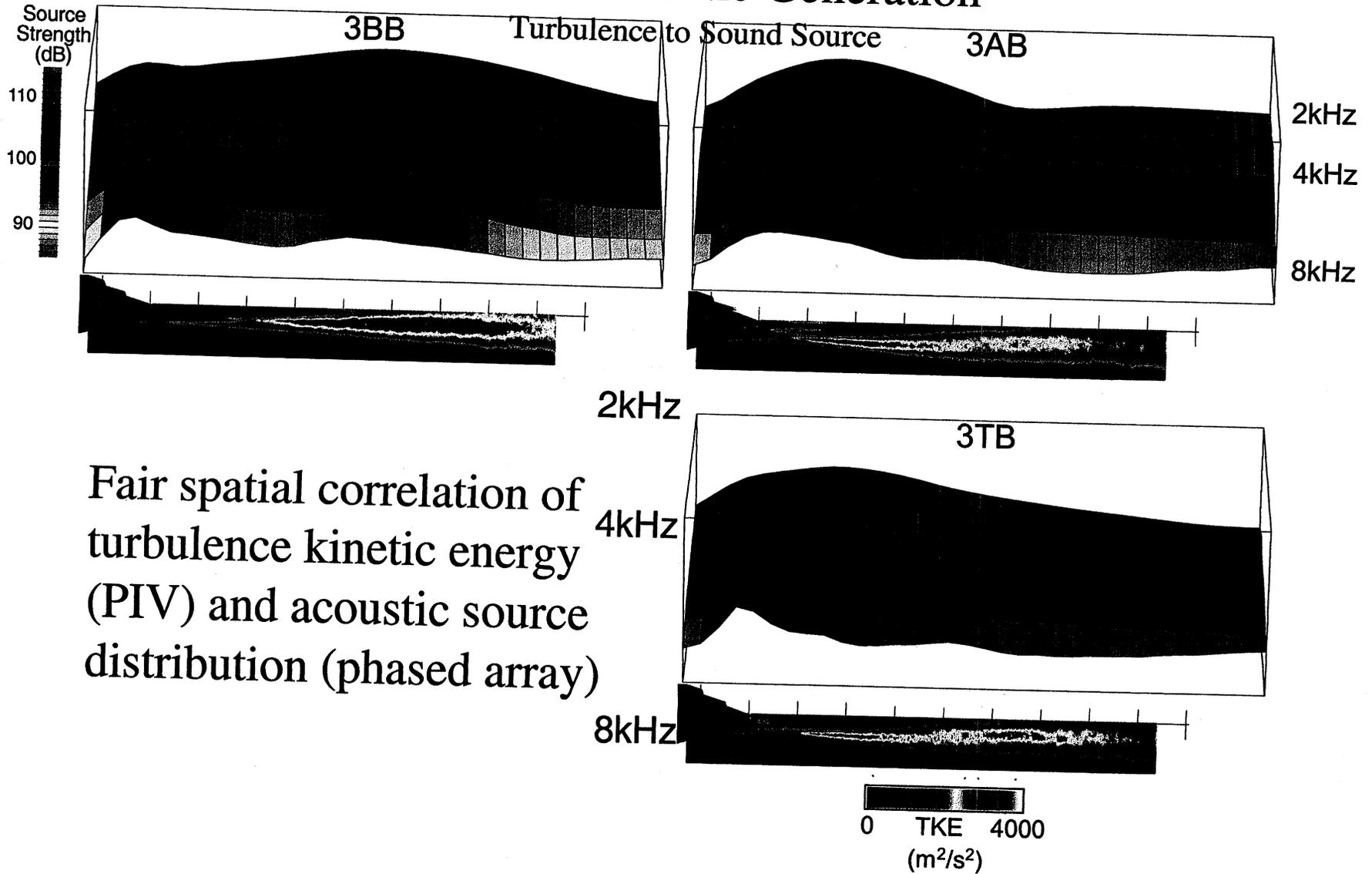
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SFNT—Acoustic Generation



Fair spatial correlation of
turbulence kinetic energy
(PIV) and acoustic source
distribution (phased array)



Conclusions

- Chevrons and tabs are effective mixing enhancement devices for jet nozzles.
- Thrust losses are small and noise modification is net reduction if done right.
- PIV allows measurement of turbulence quantities in hot, high-speed jets not available before.
- Mixing enhancement devices reduce mean velocity and turbulent kinetic energy in jet mixing region, cause some additional turbulence in first few diameters.
- Mixing enhancement devices change isotropy of turbulence (ratio of turbulence components)
- Mixing enhancement devices do not change lengthscales.
- Local homogeneity is good assumption, even in enhanced mixing nozzle flows.